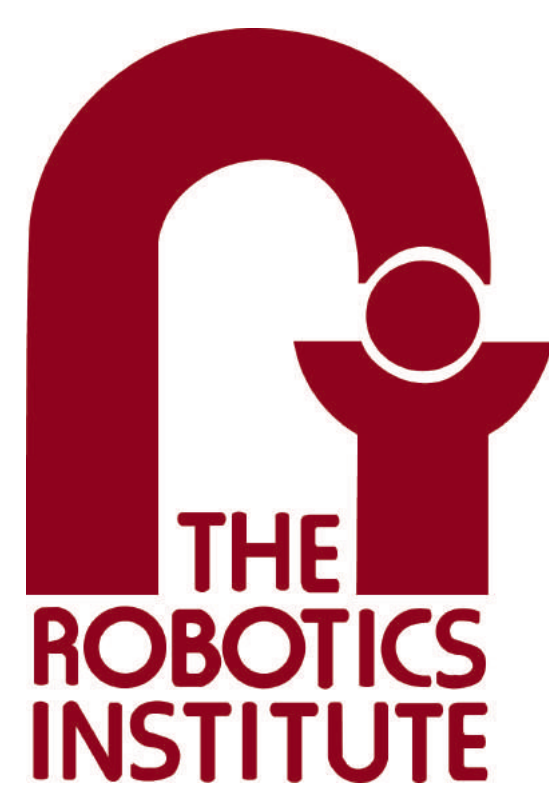


# Central Pattern Generator with Inertial Feedback for Stabilized Locomotion in Unstructured Terrain

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## Introduction

Legged animals of varying sophistication subconsciously navigate extreme terrain with ease. In an effort to match this performance, bio-inspired control mechanisms have been widely studied, but have most commonly been used for open-loop gait generation. To improve locomotion in unstructured terrain, we present a method for incorporating body stabilization into a Central Pattern Generator (CPG) by adapting CPG parameters using inertial feedback.

## Results

Locomotive speed greatly improves when robot body orientation is strictly controlled.

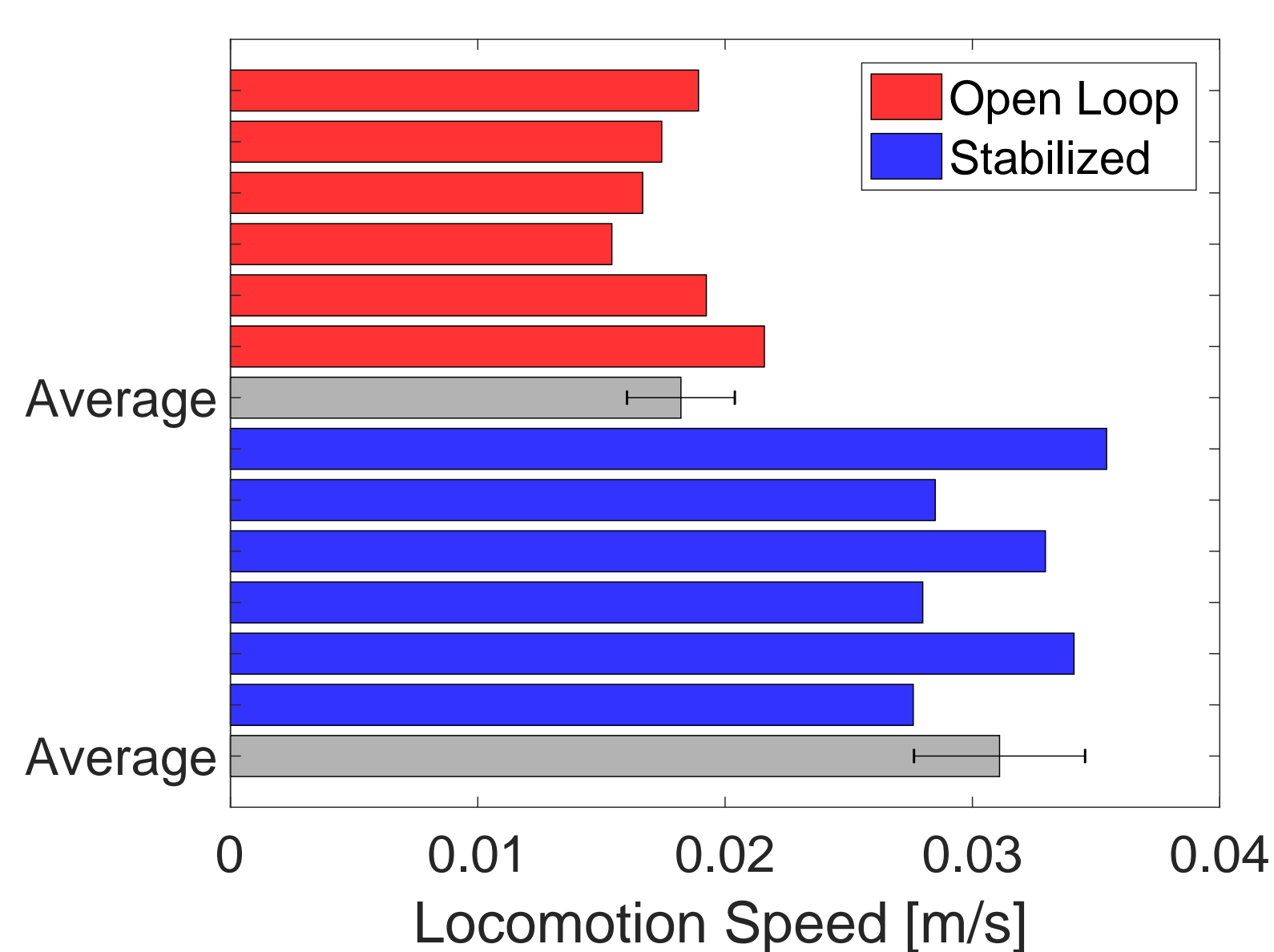


Figure 1: Performance of stabilized trials (blue) and open-loop trials (red); average values are shown in gray with overlaid standard deviations.

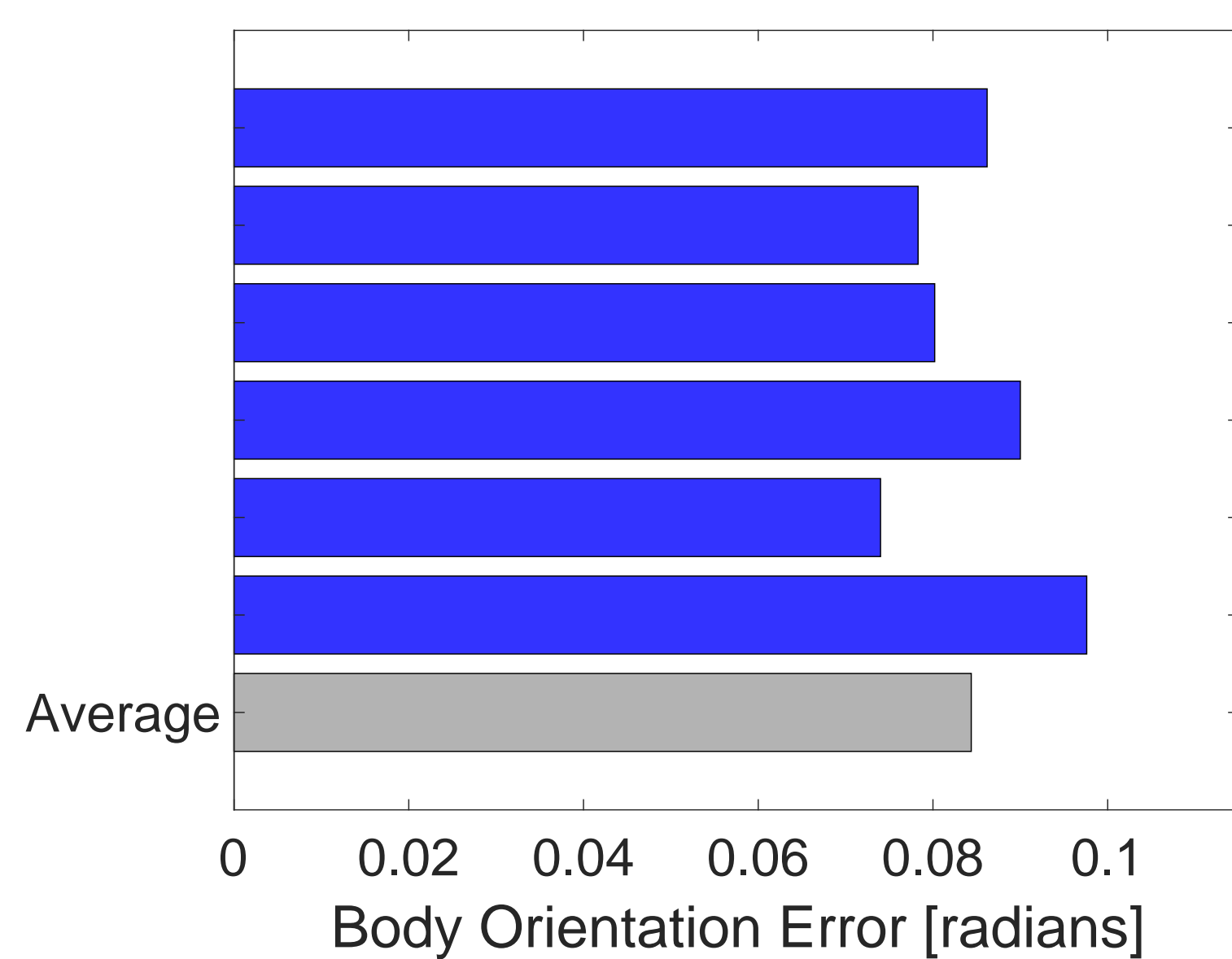


Figure 2: Body orientation error for each stabilized trial (blue), and average across all trials (gray) (shown in radians,  $\sim 5^\circ$ ).

## Conclusion

We show that inertial body stabilization improves blind locomotion by smoothing out sudden perturbations due to end-effector slip and increasing locomotive speed in unstructured terrain. Additionally, we conclude that stabilization can allow a robot to traverse steeper and more challenging terrains, where open-loop locomotion would otherwise fail. Using a CPG framework generalizes the method so that it may serve as a fundamental tool for future research on legged locomotion or a potential building block for vision-based applications.

## References

- [1] Ludovic Righetti and Auke Jan Ijspeert. Pattern generators with sensory feedback for the control of quadruped locomotion. In *Robotics and Automation, 2008. ICRA 2008. IEEE International Conference on*, pages 819–824. IEEE, 2008.

## Hexapod Robot



Figure 3: Experimental Platform: modular, series-elastic hexapod robot aerial view (left); hexapod robot leg joint configuration (right).

## Central Pattern Generator Model

We model the CPG as a dynamical system of linked oscillators in the joint space, where  $x = [x_1, \dots, x_n]$  represents the angles of the proximal, lateral joints and  $y = [y_1, \dots, y_n]$  represents the angles of distal, vertical joints:

$$\begin{cases} \dot{x}_i = \gamma(1 - \frac{(x_i - c_{x,i})^2}{a^2} - \frac{(y_i - c_{y,i})^2}{b^2}) \cdot (x_i - c_{x,i}) - \omega \frac{a}{b} \cdot (y_i - c_{y,i}) \\ \dot{y}_i = \gamma(1 - \frac{(x_i - c_{x,i})^2}{a^2} - \frac{(y_i - c_{y,i})^2}{b^2}) \cdot (y_i - c_{y,i}) - \omega \frac{b}{a} \cdot (x_i - c_{x,i}) + \lambda \sum K_{ij}(y_i - c_{y,i}) + \Delta\theta_{e_{2,i}} \end{cases} \quad (1)$$

## Inertial Stability

By examining the orientation of the robot's body, we obtain  $e \in \mathbb{R}^{3 \times n}$ , the error in end-effector position in Cartesian space for each leg:

$$e = \begin{bmatrix} x_1 & \cdots & x_n \\ y_1 & \cdots & y_n \\ z_1 & \cdots & z_n \end{bmatrix}. \quad (2)$$

Rearranging the kinematics equation,

$$\dot{x} = J\dot{\theta}, \quad (3)$$

where  $\dot{x}$  is the end effector velocity,  $J$  is the Jacobian, and  $\dot{\theta}$  is the angular speed of the joint, we obtain:

$$\Delta\theta_e \approx J^{-1}e. \quad (4)$$

In order to ensure that joint angle correction does not diverge, we add a constant dissipation to the origin:

$$\Delta\theta_e = \Delta\theta_e - \alpha \cdot \theta_e, \quad (5)$$

where  $\alpha \in \mathbb{R}$  governs the dissipative term.

By integrating the error in joint angle, denoted  $\Delta\theta_e$ , with respect to time,

$$\theta_e = \int_0^t \Delta\theta_e dt, \quad (6)$$

we obtain joint offsets,  $\theta_e$ , that correspond to the desired corrections in the orientation and height of the robot's body.

The second row of  $\Delta\theta_e$  gives offsets for the distal, vertical joints, which are used to set  $c_y$  to obtain stability:

$$c_{y,i} \equiv \theta_{e_{2,i}}. \quad (7)$$

## Experimental Setup

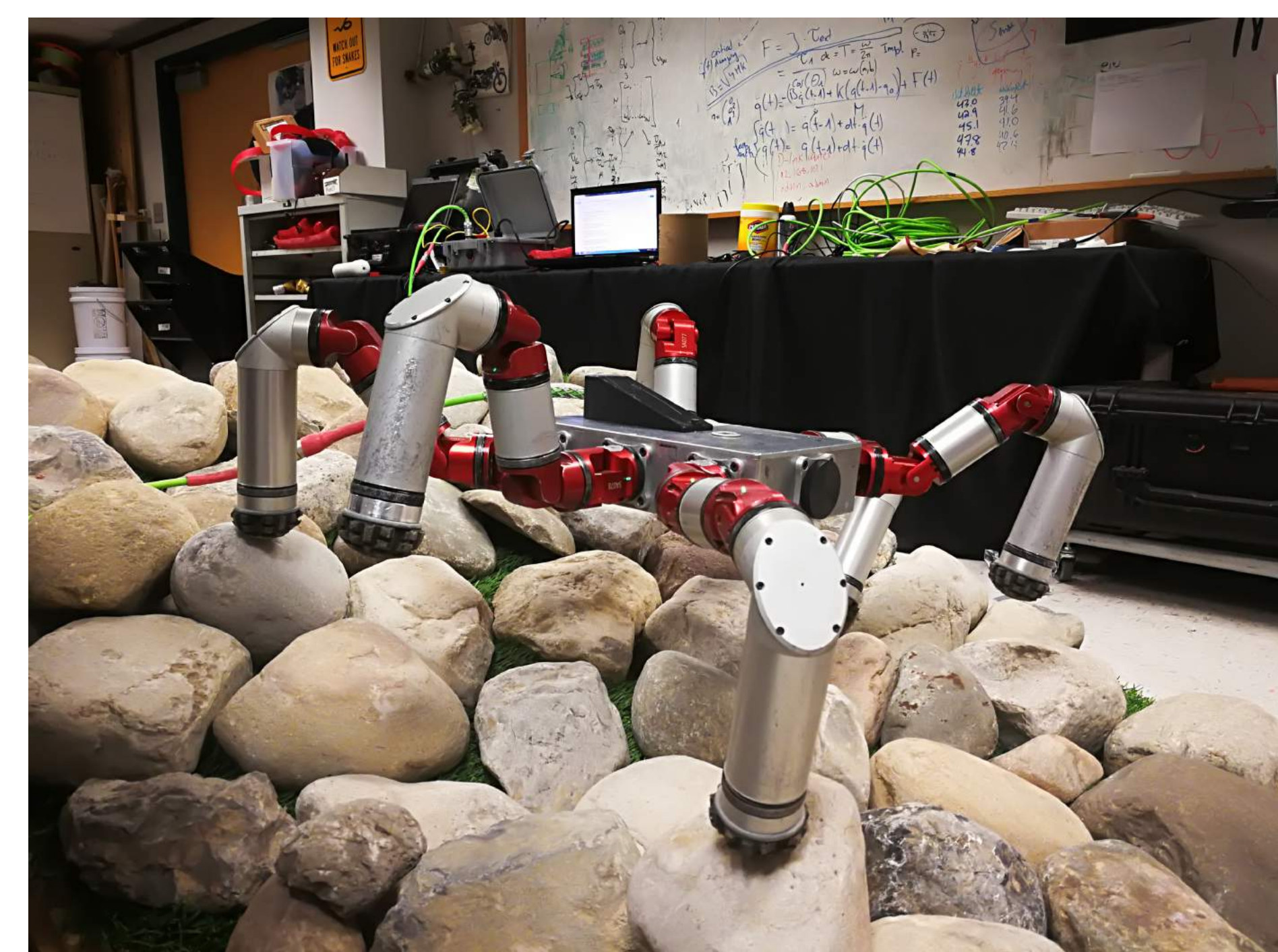


Figure 4: Hexapod robot on experimental unstructured terrain.

Experiments were conducted on a twelve-degree slope, featuring randomly-placed and -oriented rocks that varied in elevation from approximately 5cm to 20cm.

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